

Surface Subsidence Induced by Groundwater Drainage Tunneling in Granite Residual Soils (Burata Railway Tunnel, Spain)

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Abstract: Underground tunneling, besides raising geotechnical challenges, can often modify the hydrological regime around an excavated area. This fact entails not only the modification of superficial aquifers but also the appearance of subsidence phenomena as a consequence of the decrease in pore pressure. In the end, this may jeopardize the structural integrity of the construction, leading to delays and undesirable secondary effects. This paper documents the problems arising from the construction of a railway tunnel for a high-speed train in the province of Orense in the northwest of Spain. The tunnel was excavated through a highly weathered granitic massif using conventional methods. The drawdown in the water table caused by the tunnel advance was analyzed and monitored. The initial lowering of the water level was followed by a period of soil subsidence with deflections reaching up to 104 mm. These differential settlements happened along a 150-m strip on both sides of the tunnel axes, which affected urbanized areas. The topographic downfall was located ahead of the perforation head; however, it occurred after the lowering of the water table as an immediate consequence. DOI: [10.1061/\(ASCE\)GT.1943-5606.0000805](https://doi.org/10.1061/(ASCE)GT.1943-5606.0000805). © 2013 American Society of Civil Engineers.

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Introduction

The excavation of the Burata tunnel in the northwest of Spain below the groundwater level through a strongly weathered granite massif induced the drawdown of the water table to the excavation level. The superficial aquifers emptied along a 150-m strip of land on both sides of the tunnel lineation, reducing the water supply in the surrounding towns. The ground also suffered settlements of up to 104 mm in the same area prior to the advance of the tunneling works. This is attributed to consolidation of the weathered layers of the granite when the water table drops. There are abundant references related to this problem, both in the field of tunneling (Lee et al. 2009; Sinclair and Norfolk 2001; Shin and Potts 1998, 2001; Yoo et al. 2007, 2008) and in the overexploitation of aquifers (Zhang et al. 2007; Feng et al. 2008; Tomás et al. 2010). However, there is scarce literature on the

evaluation of the problem in weathered granites (Shin and Lee 2001; Forth 2004; Shin et al. 2005). The Burata tunnel is part of a high-speed railway line in Spain between Madrid and Santiago [Fig. 1(a)]. It consists of a pilot tunnel and a 3,998-m-long main tunnel with 13- and 90-m² cross sections, respectively. The tunnel was planned for an average depth of 93 m [Fig. 1(b)], with a maximum overburden of 141 m, and was excavated from two excavation shafts following the new Austrian tunneling method (NATM) between June 2006 and May 2010. The pilot tunnel advanced ahead of the main excavation by an average of 180 m. Support was implemented through bolts, shotcrete reinforced with steel ribs, and micropilot umbrellas in the tunnel portal and in areas with special problems.

Geological and Geotechnical Studies

The tunnel runs beneath an area where granites outcrop on the surface. Among the granites there is an abundance of metasediments, veins, and quartz dikes. On top of the granite substrate, an important alteration developed with a dissimilar grade of evolution at depths that reach several tens of meters, reaching a maximum in the topographic lows [Fig. 1(b)]. The preparatory geotechnical study for the Burata tunnel project consisted of a prospection of the land that included a detailed geological mapping at a scale of 1:2,000, the description of 31 geomechanical stations, and the drilling of 27 boreholes [Figs. 1(a) and (b)]. In addition, a geochemical, petrographic, and mineralogical study was also performed on 30 samples taken from the boreholes. Thin-section samples were prepared and analyzed with an electron probe. The results led to the definition of the following three geological units [Fig. 1(b)]: (1) fresh granite (FG), consisting of peraluminous granite of two unweathered micas of medium-to-fine grain; (2) metasediment (MS), consisting of mica schist, quartz schist, and paragneiss; and (3) granite residual (GR)

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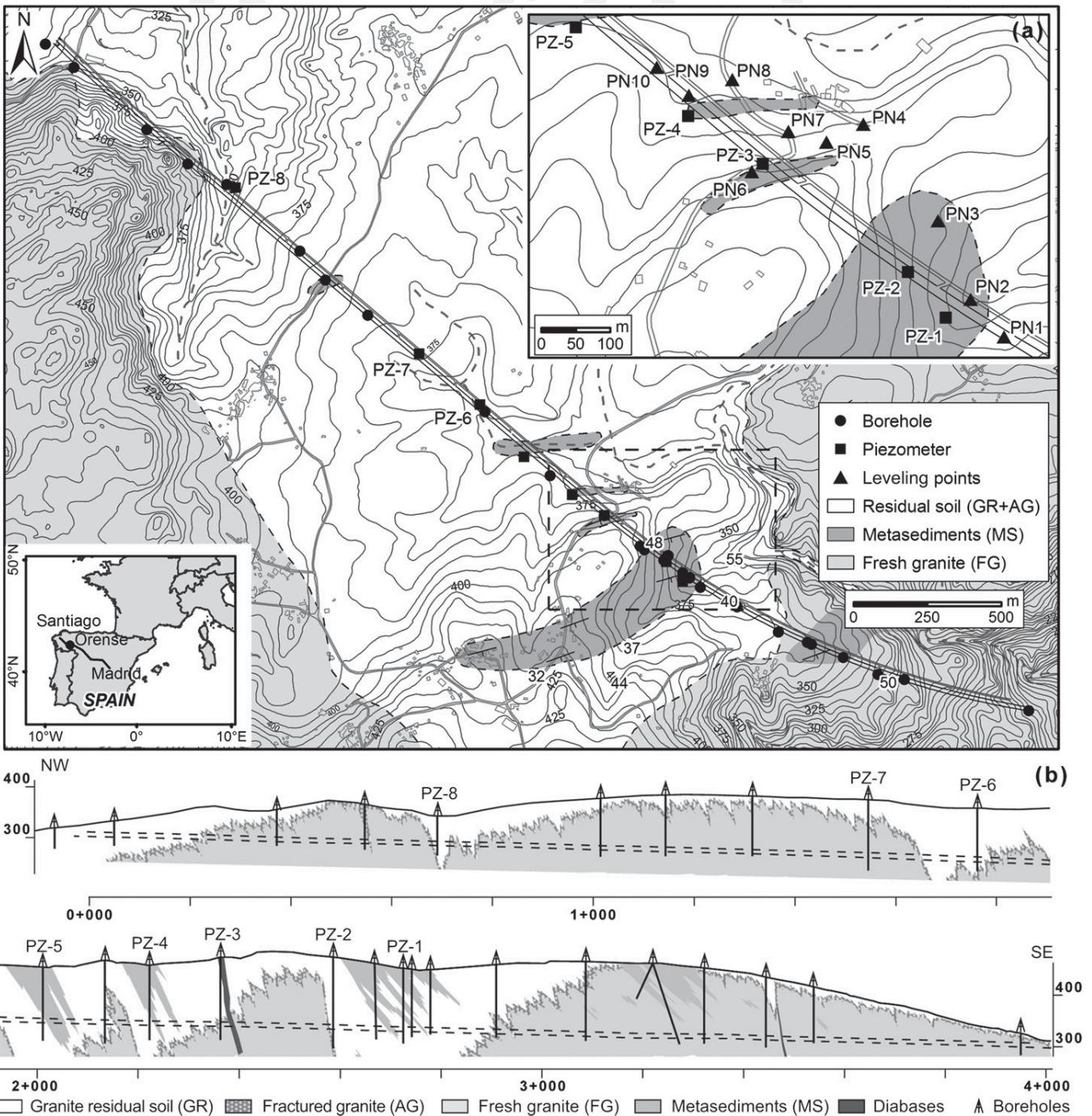


Fig. 1. (a) Geographic location and geological map of the Burata tunnel (also shown are the locations of the drill holes, leveling points, and piezometers; the upper inset is shown as an enlargement of the central part of the tunneling trace) and (b) Geological cross section along the trace of the Burata tunnel

soil generated by the destruction of certain minerals as a consequence of oxidation and hydration processes derived from the groundwater action.

Groundwater Evolution

The granite residual soil behaves as an unconfined aquifer delimited by unweathered bedrock acting as an impermeable layer. Its

hydrological behavior is determined by the grain-size distribution, with the variable content of clays and sands affecting the permeability (generally, between 10^{-3} m/day for the more clayed facies and 1 m/day for the coarse sands, estimated by the Lefranc test). During the excavation the hydrological behavior of the massif was measured by eight piezometers situated along the tunnel alignment [Fig. 1(a)], together with the monitoring of more than 200 shallow wells. In five of the piezometers (PZ-1–PZ-5) a lowering of the water table was observed (Fig. 2), in which the lowering reached

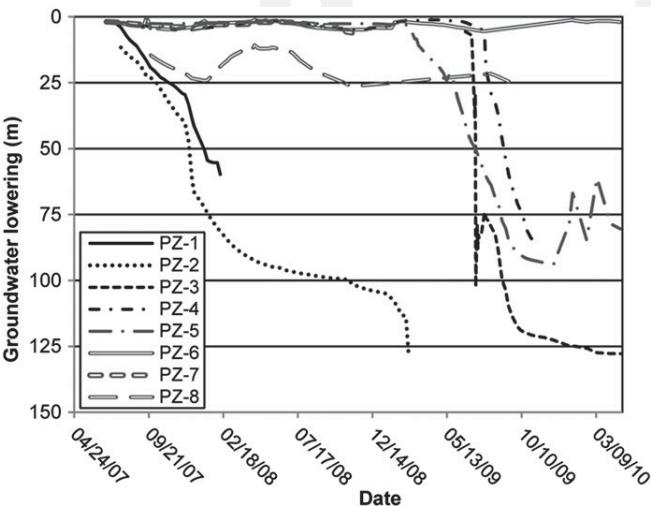


Fig. 2. Evolution of the water table observed in the piezometers during the tunnel work from April 2007 to April 2010

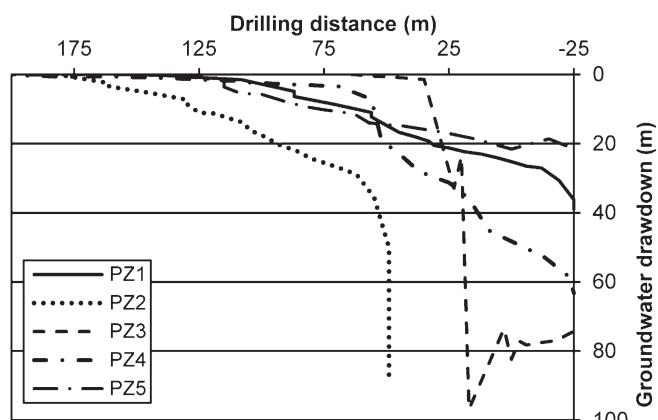


Fig. 3. Drawdown of the water table related to the distance of the perforation head for each of the piezometers

the tunnel level. The drawdown was produced at a velocity that ranged between 0.2 and 1 m/day, with the drawdown always starting before the tunnel excavation reached the piezometer, and with a distance to the pilot tunnel advancing the face between 70 and 175 m (Fig. 3). In contrast to this, PZ-6–PZ-8 showed less significant lowering of the water table (Fig. 2) because of their situation inside the fresh granite.

Subsidence Analysis

The analysis of the subsidence associated with the excavation was performed through topographic leveling, with 10 control points located in the zone of the tunnel outline [Fig. 1(a)]. The measurements (with a maximum error estimated at 10 mm) were performed weekly from 2007 to 2010. In all of the measuring points settlements were observed, with ground subsidence ranging between 32 and 104 mm (Fig. 4). An estimate of the subsidence rate oscillated between 0.2 and 0.9 mm/day. The observed subsidence affected a part of the terrain at least 150-m north of the tunnel. The settlements started after the lowering of the water table.

Discussion and Conclusions

From the data recorded throughout the excavation of the tunnel, it can be deduced that the surface subsidence observed around the Burata tunnel was mainly caused by the generalized drawdown in the water table as a result of tunnel drainage, with the excavation process being a negligible factor in the final topographic drop. The advance of the tunneling work through the most weathered parts of the granite massif caused the water to flow toward the excavation, affecting an area of 70–175 m ahead of the pilot tunnel advancing face. This range of distances is a direct consequence of the various degrees of permeability in the granite residual soils (which are grain-size dependent). Moreover, the fall in the level of the water table led to consolidation of the soil. This fact is reflected in the appearance of the settlements in the topographic profile, whose magnitude reached up to 104 mm. These settlements are proportional to the relative thickness of the weathered layer of the granite affected by the water table variation and have been estimated to be 0.8 mm/m.

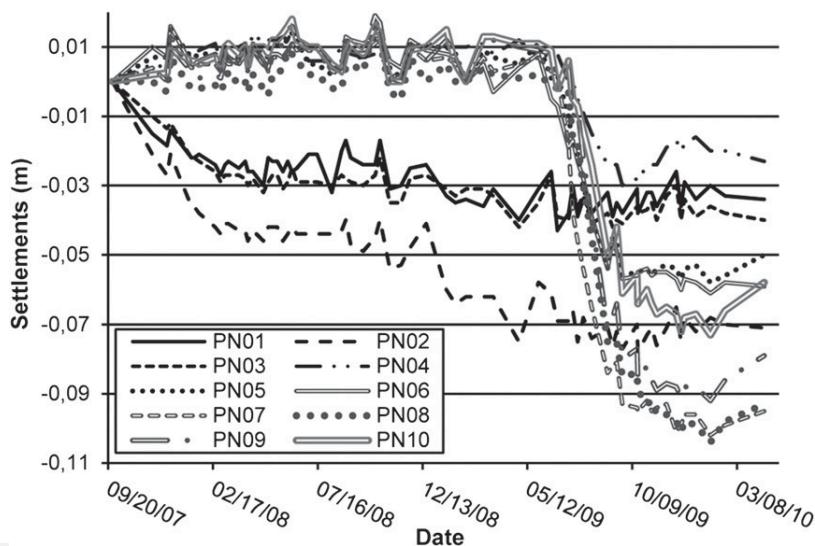


Fig. 4. Settlements measured in the leveling points [their location is shown in Fig. 1(a)]

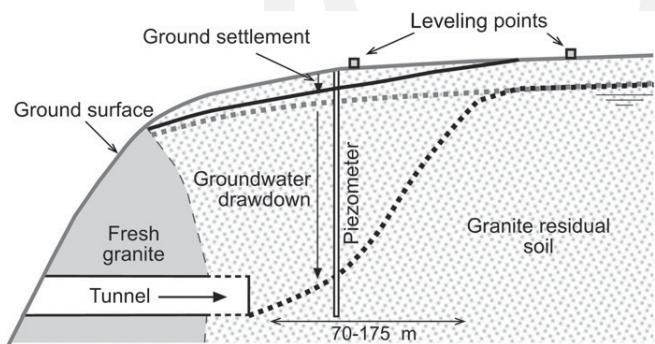


Fig. 5. Model of the subsidence processes caused by the water table drawdown

This case has been the first one to be monitored in Spain (where there are more than 1,500 km of railway and road tunneling), and is comparable to the Seoul Underground, where settlement values reached 160 mm, with a drawdown in the water table of 16 m for a typical thickness cover of 15–40 m (Yoo et al. 2008). The values obtained for the settlements induced here can be compared with those related to the overexploitation of aquifers. One example is the city of Murcia, Spain, where average settlements of 76 mm were caused by the generalized lowering of the water table by 25 m (Tomás et al. 2010), or the case of Changzhou, China, with settlements of 600 mm related to a water drawdown of 20 m (Wang et al. 2009).

In conclusion, subsidence processes related to lowering of the water table can be expected in all excavations occurring in weathered rock massifs or in permeable soils where water flow runs into the excavation (Fig. 5). The water drawdown implies a reduced pore pressure that is translated toward the surface, inducing various settlement problems. These settlements are also instantaneous when there is not a large amount of clay, as is this here. The quantification and prediction of the subsidence phenomena depend on several variables; i.e., the weathering grade of the massif, the thickness of the residual soil, the magnitude of the drop in the water table level, the excavation method, and the distance to the excavation advancing face.

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