

THz nanofocusing with cantilevered THz-resonant antenna tips

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We developed THz-resonant scanning probe tips, yielding strongly enhanced and nanoscale confined THz near fields at their tip apex. The tips with length in the order of the THz wavelength ($\lambda = 96.5 \mu\text{m}$) were fabricated by focused ion beam (FIB) machining and attached to standard atomic force microscopy (AFM) cantilevers. Measurements of the near-field intensity at the very tip apex (25 nm radius) as a function of tip length – via graphene-based (thermoelectric) near-field detection - reveal their first and second order geometrical antenna resonances for tip length of 33 and 78 μm , respectively. On resonance, we find that the near-field intensity is enhanced by one order of magnitude compared to tips of 17 μm length (standard AFM tip length), which is corroborated by numerical simulations that further predict remarkable intensity enhancements of about 10^7 relative to the incident field. Because of the strong field enhancement and standard AFM operation of our tips, we envision manifold and straightforward future application in scattering-type THz near-field nanoscopy and THz photocurrent nano-imaging,

34 nanoscale nonlinear THz imaging or nanoscale control and manipulation of matter employing
35 ultrastrong and ultrashort THz pulses.

36

37 Terahertz (THz) radiation (1) (2), loosely defined between 0.1 and 10 THz (wavelength $\lambda =$
38 $3000 - 30 \mu\text{m}$) (1), can access vibrational and rotational resonances in molecules (3) (4) (5) and
39 low-energy dynamic processes in solid-state matter or devices (4) (6) (7). For many applications,
40 a strong THz field concentration is required, for example, for high-resolution THz imaging or for
41 THz sensing of small amounts of matter (1) (3). This can be accomplished by focusing THz
42 radiation using far-field optics. However, the focal spot size is limited by diffraction to about
43 $\lambda/2 = 15 - 1500 \mu\text{m}$. A nanoscale field confinement can be achieved by concentrating THz
44 radiation with the use of metal antennas (8), sharp metal wires (9) (10) (11) (12) (13), or
45 subwavelength apertures or slits (12) (14) (15) (16). In particular, the THz field concentration at
46 a sharp tip apex can be achieved by exploiting the lightning rod effect, or by adiabatic
47 compression of an electromagnetic wave propagating along a long, tapered metal wire (10) (11)
48 (13) (17) (18) (19). Field confinements as large as $\lambda/4600$ have been already reported (20).
49 Applications of near-field enhancement at nanoscale metal tips include the THz control of
50 photoemission (21), nanoscale-resolved THz scattering-type scanning near-field microscopy (s-
51 SNOM) (22) (23) (24) (25), ultrafast sub-cycle THz nano-spectroscopy (26) or THz photocurrent
52 nanoscopy (27).

53

54 In many applications, the illuminated metal tip is much longer than the THz wavelength λ , in
55 order to guarantee strong near-field enhancements and scattering from the tip. For
56 subwavelength-scale THz imaging, the rather long tips of a scanning tunneling microscope

57 (STM) (28) (29) (30) can be employed. In case of non-conducting samples, the long metal tips
58 can be scanned over the sample surface via shear-force control that utilizes a tuning fork (31)
59 (32). Alternatively, the tips of standard AFM cantilevers may be used for THz near-field imaging
60 (24) (26). While this approach can be performed with standard and easy-to-use AFM
61 instrumentation, the AFM tips suffer from low field enhancement due to the large mismatch
62 between tip length ($\ll \lambda$) and THz wavelength λ . AFM tips of a length in the order of the THz
63 wavelengths - potentially exhibiting geometric antenna resonances that provide large field
64 enhancements - have not been developed yet, despite their advantage to enable nanoscale THz
65 control and imaging applications based on widely available AFM instrumentation.

66

67 Here, we developed cantilevered antenna probes with nanoscale tip apex for resonant
68 nanofocusing of THz radiation. Their lengths were designed to support antenna modes to
69 resonantly enhance the THz field at the tip apex. We attached the antennas to standard atomic
70 force microscopy (AFM) cantilevers to allow for a precise control of the position of the THz
71 hotspot on a sample surface using standard AFM instrumentation. To characterize the antenna
72 probes, we measured the near field intensity directly at the tip apex using a graphene-based THz
73 photodetector (27) (33), rather than deducing it by detecting the tip-scattered light in the far field.
74 We find that our tips support antenna resonances and corroborate our findings with numerical
75 simulations and antenna theory.

76

77 Fig. 1a shows a false color scanning electron microscopy (SEM) image of a FIB fabricated
78 THz antenna probe using a Helios 450 DualBeam (FEI, Netherlands) electron microscope (34)
79 (35). A detailed description of the fabrication process is given in the supplement. We used

80 standard Si AFM cantilevers (Nanoworld, Switzerland) and replaced the original tip by a several
81 tens of micrometers long tip made of an 80/20 Pt/Ir alloy. To achieve a high field confinement
82 and enhancement, the tip apex diameter is adjusted to only (50 ± 3) nm. We fabricated six
83 different tips with lengths $17\mu\text{m}$, $33\mu\text{m}$, $43\mu\text{m}$, $55\mu\text{m}$, $65\mu\text{m}$, and $78\mu\text{m}$, each of which supports
84 a different antenna mode at one given excitation THz wavelength.

85

86 To characterize the cantilevered THz antennas, we employed them as scanning probe tips in a
87 scattering-type Scanning Near-field Optical Microscope (s-SNOM, Neaspec GmbH, Germany).
88 The s-SNOM is based on a non-contact atomic force microscope (AFM), where the tip is
89 oscillating vertically at the mechanical resonance frequency Ω of the cantilever. In the present
90 work, the oscillation amplitude was 40 nm. The tips were illuminated with the focused THz
91 beam ($\lambda = 96.5 \mu\text{m}$, 3.11 THz) of a gas laser (SIFIR-50 FPL, Coherent Inc., USA), which
92 provides monochromatic radiation up to 100 mW power. In contrast to standard s-SNOM, we did
93 not detect the tip-scattered field but used a graphene-based THz detector (27) (36) (illustrated in
94 Fig. 1b and described in the Methods section) to measure the near-field intensity directly at the
95 tip apex. The detector, in brief, consists of a graphene sheet encapsulated in two hexagonal
96 Boron Nitrite (h-BN) layers on top of two laterally separated gates G_L and G_R . By applying two
97 different gate voltages V_L and V_R , we generated a pn-junction in the graphene across the gap
98 between the two gates. The near fields at the tip apex locally heat the electrons in the graphene,
99 which induces close to the junction a thermoelectric photocurrent (27) (36) (37) (38). This
100 photocurrent can be measured through the two lateral contacts C_L and C_R , and is found to be
101 proportional to the near-field intensity for the power applied in our experiments, as shown in the
102 inset in Fig. 2b (see also supplement). We note that the direct detection of the tips' near field

103 offers the advantage that only the tip illumination needs to be adjusted. There is no need for a
104 detection beam path, which typically comprises an interferometer (39) that requires not only
105 accurate adjustment of the collection and detector optics, but also of the beam quality and
106 wavefronts. This significant reduction of adjustment steps enables a more reliable and accurate
107 comparison of the near-field enhancement at the apex of various different tips.

108

109 We first demonstrate that the antenna probes allow for stable AFM imaging and nanoscale THz
110 focusing. To that end, we recorded a topography image (Fig. 1c) of the detector device (using the
111 $78 \mu\text{m}$ long antenna probe), showing the top surface (h-BN layer) of the detector above the
112 active region, as well as the lateral Au contacts (left and right) collecting the photocurrent. It
113 clearly verifies a stable AFM operation using our THz antenna probes, despite their comparably
114 large size and hence mass ($\sim 60 \text{ pg} > 80$ times the mass of standard Si tip), which reduces the
115 mechanical cantilever resonance frequency by nearly a factor two (from 252 kHz for cantilever
116 with standard Si tip to 139 kHz with THz antenna probe of length $78 \mu\text{m}$). To demonstrate the
117 THz nanofocusing functionality of the antenna probe, we recorded a DC photocurrent image
118 $I_{\text{PC,DC}}$ (Fig. 1d) simultaneously to the topography. We see a bright vertical stripe of strong
119 photocurrent $I_{\text{PC,DC}}$ in the image center, which reveals the strong photo-thermoelectric current
120 generation near the pn-junction. The stripe has a sub-wavelength full width at half maximum of
121 $\sim 0.6 \mu\text{m}$, which verifies that the THz radiation can be focused by the tip to a deeply
122 subwavelength scale spot. Further, we observe a strong photocurrent $I_{\text{PC,DC}}$ close to the lateral
123 source and drain contacts. It arises from a less-defined local doping of the graphene near the
124 contacts (40) (41). The photocurrent abruptly drops to a constant background value (see
125 discussion in following paragraph) at the graphene edge (marked by the white dashed line in Fig.

126 1d) and at the metal contacts. From the signal change at the contact we estimate spatial
127 resolution (*i.e.* lateral field confinement at the tip apex) of about 100 nm ($\lambda/1000$), verifying the
128 conversion of incoming THz radiation into a highly confined nanofocus at the tip apex, and
129 hence the functionality of our tips as high-resolution THz near-field probes.

130

131 For quantifying the vertical field confinement, we recorded the photocurrent $I_{\text{PC,DC}}$ as a
132 function of distance h between tip and detector (solid red curve in Fig. 2a) at the position marked
133 by a black cross in Fig. 1e. The photocurrent $I_{\text{PC,DC}}$ decays rapidly with increasing h . For large h
134 it approaches asymptotically the constant value of 3.3 nA, which we assign to a background
135 photocurrent $I_{\text{PC,BG}}$ that is generated by the diffraction-limited illumination of the whole device.
136 Knowing $I_{\text{PC,BG}}$, we can extract the near-field contribution $\Delta I_{\text{PC}} = I_{\text{PC,DC}} - I_{\text{PC,BG}}$ to determine
137 vertical confinement ($1/e$ decay length d) of the THz near field (Fig. 2b). We measure $d = 28$ nm,
138 revealing a deep subwavelength-scale vertical field confinement at the tip apex (amounting to
139 about $\lambda/3500$), which agrees well with the numerically calculated near-field distribution at the tip
140 apex (50 nm diameter) of a 78 μm long Pt tip (inset of Fig. 2b).

141

142 Interestingly, the background contribution ($I_{\text{PC,BG}} = 3.3$ nA) is remarkably small compared to
143 the near-field signal, $\Delta I_{\text{PC}} = 15.1$ nA, which typically is not the case in scattering-type and tip-
144 enhanced near-field techniques. We explain the finding by the small active area of the THz
145 detector, which is significantly smaller than the THz focus illuminating the tip. The small but
146 non-negligible background signal can be fully suppressed by demodulating the detector signal at
147 harmonics $n\Omega$ of the tip oscillation frequency Ω (similar to s-SNOM and infrared photocurrent
148 nanoscopy (24) (38) (42)), yielding the signal $I_{\text{PC,n}\Omega}$. Recording $I_{\text{PC,n}\Omega}$ as a function of tip-detector

149 distance h for $n = 1$ and 2 (dashed red curves in Fig. 2a) indeed shows that the demodulated
150 photocurrent signal completely vanishes for large tip-detector distances h . Due to the “virtual tip-
151 sharpening” effect by higher harmonic signal demodulation (43) (44), we measure a decreasing
152 $1/e$ decay length of $d_1 = 17$ nm ($\lambda/5600$) and $d_2 = 9$ nm ($\lambda/10500$) for $n = 1$ and $n = 2$,
153 respectively. The demodulation also allows for background-free photocurrent nanoimaging, as
154 demonstrated in Fig. 1e (demodulation at $n = 1$), where the photocurrent drops to $I_{\text{PC},n\Omega} = 0$ nA on
155 the lateral Au contacts and on the SiO_2 substrate (white areas in Fig. 1e).

156

157 Having verified a proper AFM operation and near-field focusing performance of the FIB-
158 fabricated tips, we compare in the following the near-field intensity at the apex of differently
159 long tips. In Fig. 2b we compare ΔI_{PC} as a function of tip-detector distance h for a $78 \mu\text{m}$ and a
160 $17 \mu\text{m}$ long tip. The measurements were taken at the same position on the photodetector, marked
161 by a black cross in Fig. 1d ($5.5 \mu\text{m}$ from the device edge along the pn-junction). While the
162 background corrected signal ΔI_{PC} at large distances h converges to zero for both tips, we observe
163 at contact ($h = 0$ nm) a significantly enhanced photocurrent for the $78 \mu\text{m}$ long tip. For more
164 detailed insights into the dependence of the near-field intensity enhancement on the tip length,
165 we performed photocurrent measurements with six differently long tips. To that end, we
166 recorded line profiles of ΔI_{PC} (average of 100, marked in Fig. 1d by dashed black horizontal line)
167 across the pn-junction. The recording of line profiles, rather than approach curves, offers the
168 advantage that measurement errors due to uncertainties in tip positioning can be minimized. Note
169 that we did not analyze the background-free demodulated photocurrent signals $I_{\text{PC},n\Omega}$, since they
170 do not reveal the near-field intensity but the vertical gradients of the near-field intensity. In Fig.
171 3a we plot three line profiles showing the near-field photocurrent ΔI_{PC} obtained with tips of

172 length $L = 17 \mu\text{m}$, $33 \mu\text{m}$, and $78 \mu\text{m}$. All three curves exhibit a maximum near-field
173 photocurrent $\Delta I_{\text{PC,max}}$ at the position of the pn-junction ($x = 0 \text{ nm}$), and decay to either side
174 towards the source and drain contacts. As seen before in Fig. 2b, we find a strong variation of the
175 near-field photocurrent for the different tips. Plotting $\Delta I_{\text{PC,max}}$ as a function of antenna length L
176 for the six different tips (blue dots in Fig. 3b), we find that $\Delta I_{\text{PC,max}}$ strongly depends on the tip
177 length L , indicating minima and maxima and thus antenna resonances. The longest antenna
178 probe ($L = 78\mu\text{m}$) yields the strongest, nearly nine-fold near-field intensity enhancement
179 compared to the shortest tip ($L = 17 \mu\text{m}$). Note that both the tip length and the tip apex diameter
180 determine the photocurrent signal. A larger tip diameter reduces the lateral field confinement
181 below the tip, thus illuminating the detector on a larger area, while the field enhancement is
182 reduced. For a constant tip diameter it can be shown that a variation of the tip length only varies
183 the field enhancement but not the field confinement (see supplement S4). Hence, we can isolate
184 the effect of the antenna length (field enhancement) on the photocurrent by adjusting the apex
185 diameter for each tip to a constant value. For the presented experiments, we fabricated tips with a
186 diameter of 50 nm , which was highly reproducible with an accuracy of $\pm 3 \text{ nm}$.

187

188 To elucidate the variations of the near-field enhancement for different tips, we performed
189 numerical full-wave simulations (see Methods) of tips, illuminated with THz radiation, with a
190 geometry as depicted in Fig. 3c (for more detail see schematics D in Fig. 4a). We assume a p-
191 polarized plane wave illumination (electric field E_{inc}) at 3.11 THz ($\lambda = 96.5 \mu\text{m}$) at an angle of α
192 $= 60^\circ$ relative to the tip axis. The tip (with small Si cantilever attached at its shaft) is placed $h =$
193 20 nm above the surface of a detector consisting of a 9 nm thick hBN layer that covers a
194 graphene layer on top of a bulk hBN substrate. The blue curve in Fig. 3b shows the calculated

195 near-field intensity enhancement $f = \left(\frac{E_{nf}}{E_{in}}\right)^2$ between tip and hBN surface (10 nm below the tip).
196 An excellent agreement with the experimentally measured near-field photocurrent (blue dots) is
197 observed. Particularly, the calculation exhibits the maxima at tip lengths of about $L_{res,1} = 34 \mu\text{m}$
198 and $L_{res,2} = 81 \mu\text{m}$. The logarithm of the near-field distributions shown in Fig. 3d let us identify
199 the maxima as first and second order antenna resonance, respectively. The latter is excited
200 because of retardation along the tip axis, caused by the inclined illumination relative to the tip
201 axis (45). The two resonances yield an impressive field intensity enhancement of about 1.2×10^7
202 and 2×10^7 . Most important, the resonant tips increase the field intensity enhancement by about
203 one order of magnitude compared to the $17 \mu\text{m}$ long tip, which length is that of standard AFM
204 tips.

205
206 Compared to classical dipolar radio wave antennas (45) – where $L_{res,n} = n \lambda/2$ with n being
207 the resonance order – we find that i) the antenna tip’s resonances occur at shorter lengths, and ii)
208 their resonance lengths do not scale linearly with n (we measure $L_{res,1} = \lambda/2.82$ and $L_{res,2} = \lambda/1.19$)
209 These deviations may be explained by resonance shifts caused by the presence of the cantilever
210 and/or photodetector. To understand the resonance shifts and to establish future design rules for
211 resonant THz probes, we performed simulations considering a systematic variation of the tip’s
212 environment. First, we calculated the near-field intensity enhancement 10 nm below the apex of
213 an isolated antenna tip (illustrated by sketch A in in Fig. 4a) as a function of the tip length (black
214 curve, Fig. 4b). In good agreement with classical antenna theory (45) ($L_{res,n} = n \lambda/2$), we find the
215 first two antenna resonances at $L_{res,1} = 44 \mu\text{m} = \lambda/2.19$ and $L_{res,2} = 89 \mu\text{m} = \lambda/1.08$. The small
216 deviation from $L_{res,n} = n \lambda/2$ we explain by the conical shape of the tip (45). By adding a silicon
217 cantilever to the tip shaft (sketch B in Fig. 4a), the resonance length of the calculated spectrum

218 (red curve in Fig. 4b) shift to $L_{\text{res},1} = 34 \mu\text{m} = \lambda/2.8$ and $L_{\text{res},2} = 81 \mu\text{m} = \lambda/1.2$, while the peak
219 height is reduced by about 27 and 17 percent, respectively. Both observations can be explained
220 by a capacitive loading of the tip antenna by the Si cantilever (45). Next, the sample (detector
221 device) is considered in the simulations (sketch C in Fig. 4a). It is placed 20 nm below the tip
222 apex, and the field enhancement is measured 10 nm below the tip. A detailed description of the
223 simulation parameters is given in the methods section. The calculated spectrum is shown by the
224 blue curve in Fig. 4b. Compared to geometry B (red curve in Fig. 4b), the near-field intensities at
225 the resonance lengths $L_{\text{res},1}$ and $L_{\text{res},2}$ are significantly enhanced by a factor of about seven. This
226 enhancement can be explained by the near-field coupling between tip and sample. Interestingly,
227 the near-field coupling does not further shift the antenna resonance, which typically occurs at
228 visible and infrared frequencies when an antenna is brought in close proximity to a dielectric or
229 metallic sample (46).

230

231 To better understand the absence of resonance shifts due to tip-sample coupling, we first
232 studied the role of the graphene in the near-field coupling. We repeated the numerical
233 calculation, but replaced the graphene with a perfect electric conductor (PEC) (geometry D in
234 Fig. 4a). Although the PEC perfectly screens the near fields at the tip apex, the antenna spectrum
235 (gray curve, Fig. 4b) shows only a minor increase of the peak heights of about twenty percent,
236 and a minor resonance length shift ($L_{\text{res},1} = 33.5 \mu\text{m} = \lambda/2.9$ and $L_{\text{res},2} = 80.5 \mu\text{m} = \lambda/1.2$)
237 compared to geometry C (blue curve, Fig. 4b). The results imply that graphene at THz
238 frequencies acts as a nearly metallic reflector for the tip's near fields. The results imply that
239 graphene at THz frequencies acts as a nearly metallic reflector for the tip's near fields. This can
240 be explained by the convergence of the Fresnel reflection coefficient towards one for the large

241 wavevectors associated with the near fields at the tip apex (47). Consequently, strong near-field
 242 coupling between tip and graphene occurs, leading to strongly enhanced field at the tip apex. In
 243 this regard, the nearly negligible spectral shift of the antenna resonance may be even more
 244 surprising.

245

246 We explain the negligible spectral shift with the help of radio frequency (RF) theory (45). In
 247 the RF range, circuit theory is an essential tool for the efficient design of antennas, and has
 248 recently been adopted for the visible and infrared spectral range (48) (49) (50). We consider the
 249 tip above the sample as an antenna arm (for simplicity a thin metal rod) above a metallic ground
 250 plane. A sketch and the corresponding circuit model are shown in Figs. 5a and b. The antenna
 251 arm (rod above) is described by its intrinsic (dipole) impedance, $Z_A = R_A + i X_A$, where R_A and
 252 X_A are the dipole's resistance and reactance, respectively (see Fig. 5d) (45). The air gap between
 253 tip and sample can be considered as a capacitive load with impedance given by (48)

254

$$Z_{gap} = R_{gap} + i X_{gap} = -\frac{ih}{\omega \epsilon D^2} \quad (1)$$

255

256 where h is the gap height, ω the THz frequency, $\epsilon = 1$ (air) the dielectric permittivity of the gap
 257 filling medium and D the diameter of both the antenna arm and the gap. Because of the open
 258 circuit operation of our antenna (the antenna is neither connected to a source nor a receiver), the
 259 input impedance $Z_{in} = R_{in} + i X_{in}$ of the antenna can be considered as a serial combination of the
 260 two impedances Z_A and Z_{gap} (49) (50) (51). In this circuit model (Fig. 5a and b), a resonance
 261 occurs when $X_{in} = 0$ (48) (52), *i.e.* when the capacitive reactance of the load cancels the intrinsic
 262 inductive reactance of the antenna, $-X_{gap} = X_A$.

263

264 To understand the antenna resonance, we discuss X_A and X_{gap} as a function of the antenna arm
265 length L . The red curve in Fig. 5c shows X_A for an illumination wavelength $\lambda = 96.5 \mu\text{m}$. It was
266 calculated according to reference (45) (see Methods), assuming a metal rod of diameter $D = 50$
267 nm (corresponding to the tip apex diameter). We find $X_A = 0$ for $L \approx \lambda/4$, which represents the
268 first closed circuit resonance of a classical RF antenna comprising a metal rod (of length L) on a
269 ground plane, not considering the air gap yet. At $L \approx \lambda/2$ we find that X_A diverges, indicating
270 the first open circuit (scattering) resonance (48). To see how the antenna resonance depends on
271 the capacitive coupling across the air gap, we plot the capacitive reactance $|X_{\text{gap}}|$ for gap heights
272 of $h = 4$ nm and 5 nm (horizontal dashed red lines in Fig. 5c). We observe that $|X_{\text{gap}}|$ decreases
273 with decreasing gap height (*i.e.* the gap capacitance increases) and the intersection between X_A
274 and $|X_{\text{gap}}|$ (resonance condition) shifts the antenna resonance length L_{res} from $\lambda/2$ towards $\lambda/4$
275 for further decreasing gap width (see also Fig. 5d). Interestingly, the resonance length $L_{\text{res}} \approx \lambda/2$
276 barely shifts until gap heights as small as 5 nm are reached. Obviously, the capacitance of an air
277 gap larger than 5 nm is negligible small and thus yields a large capacitive reactance that is
278 comparable to that of the antenna close to its open circuit resonance.

279

280 We show in Figure 5d the antenna resonance length L_{res} as a function of the gap width h (red
281 curve). For $h > 5$ nm we find that L_{res} is nearly constant and only slightly smaller than $\lambda/2$. Only
282 in close proximity to the substrate ($h < 5$ nm) the resonance length rapidly decreases. For
283 comparison, we numerically calculated the antenna resonance length of a metal tip above a
284 perfectly conducting ground plane. The result (inset Fig. 5d) confirms that the antenna resonance
285 of a tip does not shift for tip-sample distances larger than 5 nm, although the antenna resonance

286 length ($L_{\text{res}} = 44 \mu\text{m} = \lambda / 2.19$) is slightly smaller than that obtained by antenna theory (which
287 can be attributed to the conical shape of the tip, which is not considered in our antenna circuit
288 model). Based on these theoretical results we can explain the absence of resonance shifts in our
289 experiments and the numerical simulations shown in Figs. 3 and 4 by the relatively large average
290 distance $h = 30 \text{ nm}$ between tip and graphene. We conclude that in future design of THz resonant
291 probes and interpretation of results one needs to consider the possibility of resonance shifts only
292 for very small tip-sample distances depending on tip radius.

293

294 We finally discuss our results in the wider context of optical antennas. We used the antenna
295 circuit model to calculate the resonance shifts for a mid-infrared illumination wavelength ($\lambda =$
296 $9.6 \mu\text{m}$; gray curve in Fig. 5d). For the same antenna diameter D , we observe that a significant
297 shift of the resonance length L_{res} occurs already at much larger gap width h . This can be
298 attributed to the decreasing capacitive gap reactance X_{gap} when the frequency is increased (Eq.
299 1), while the inductive antenna reactance X_A barely changes (compare grey and red curves in Fig.
300 5c). We note that our calculations do not consider plasmonic effects, which at higher frequencies
301 cause further resonance shifts, although not being the root cause for them.

302

303 In summary, we have demonstrated the FIB fabrication of sharp, several tens of micrometer
304 long THz antenna tips on standard AFM cantilevers. To evaluate their performance, we applied a
305 graphene-based THz detector to measure the relative near-field intensity directly at the tip apex.
306 The tips were found to support strong antenna resonances, in excellent agreement with numerical
307 calculations. At resonance, the tips provide a nine-fold near-field intensity enhancement at the tip
308 apex as compared to tips of a length that is typical in AFM, while the numerical simulations

309 predict resonant near-field intensity enhancement factors of up to 10^7 relative to the incident
310 field. Our nanoscale THz-resonant near-field probes promise exciting future applications,
311 including scattering-type THz near-field microscopy with enhanced sensitivity, nanoscale
312 nonlinear THz imaging or nanoscale control and manipulation of matter using ultrastrong and
313 ultrashort THz pulses (53) (54) (7) (55) (56). We envision even stronger field enhancement by
314 further reducing the tip apex diameter from currently 50 nm to well below 10 nm.

315

316

317 METHODS

318 **Split-gate graphene detector**

319 The detector (27) (36) consists of a graphene sheet encapsulated between two layers (9nm top,
320 27nm bottom) of hexagonal Boron Nitride (hBN). This hBN-graphene-hBN heterostructure is
321 placed on top of two gold backgates, which are laterally separated by a gap of 150 nm. By
322 applying voltages V_L and V_R to the gates, the carrier concentration in the graphene can be
323 controlled separately. In our experiment we have chosen the carrier concentrations $n_{L/R} = +/-$
324 $2.6 \times 10^{11} \text{ cm}^{-2}$, yielding a sharp pn-junction across the gap between the two gates. When the tip is
325 placed above the gap, the near field at the apex locally heats the electrons in the graphene,
326 yielding a photocurrent I_{PC} according to $I_{PC} = (S_L - S_R) \Delta T$ (27) (57) (37). Here, ΔT is the local
327 temperature gradient below the tip and $(S_L - S_R)$ is the local variation of the Seebeck coefficient S
328 (in our device generated by the strong carrier density gradient *i.e.* the pn-junction above the gap).
329 The photocurrent I_{PC} is measured via the two lateral source and drain gold contacts. The detector
330 is operated in its linear regime (58) for the power applied in the experiments, as shown in Fig.

331 2b. Then, for fixed gate voltages, the photocurrent I_{PC} is proportional to the temperature gradient,
332 which in turn is proportional to the near-field intensity at the tip apex (38).

333

334 **Fourier Filtering of DC photocurrent signals**

335 During the measurement of the DC approach curves (Fig. 2b) and the line profiles (Fig. 3 a) a
336 periodic noise of 50 Hz could not fully be eliminated. To correct the data we used Fourier
337 analysis, where first the respective data set was Fourier transformed. In Fourier domain we
338 identified the frequency f_0 corresponding to 50 Hz and removed the respective data points. The
339 removed data points were replaced by a linear interpolation between the two adjacent points.
340 Finally, the inverse Fourier transformation of the resulting data set yields the presented DC
341 approach curves (Fig. 2b) and line profiles (Fig. 3a). To illustrate the effect of the filtering
342 procedure, we show in the supplementary Fig. S4 one filtered line profile in comparison with the
343 original data.

344

345 **Numerical Simulations**

346 The numerical simulations were conducted using the commercial software Comsol
347 (www.comsol.com, Stockholm, Sweden) based on finite element methods in the frequency
348 domain. In all simulations, the conical tip had an apex radius $R = 20$ nm and a ratio
349 length/width=8, which in good approximation represents the experimentally fabricated tips. For
350 the metal we used a dielectric permittivity of Pt $\epsilon_{Pt} = -5500 + i * 12000$ resulting from a
351 Drude model fit in reference (59). The part of the cantilever, to which the tips were attached, was
352 simulated as a piece of silicon of $6 \mu\text{m}$ thickness (obtained from SEM image) and $5 \mu\text{m}$ length
353 and width. The length and width were chosen to obtain convergence of the numerical

354 simulations. The tip was illuminated by a plane wave E_{in} with wavelength $\lambda = 96.5\mu m$ (3.11
 355 THz) at an angle of 60° relative to the tips axis. The sample was placed 20 nm beneath the tip,
 356 while the electric field enhancement E_{nf} was calculated 10 nm below the tip apex.

357 We simulated the graphene with a Fermi energy $E_F = v_f * \hbar * \sqrt{|n|} * \pi \approx 300 meV$, a
 358 relaxation time $\tau = \frac{\mu E_F}{v_f^2} \approx 1.2 ps$, with Fermi velocity $v_F = 10^8 cm s^{-1}$, and carrier sheet
 359 density $n = 6.57 * 10^{12} cm^{-2}$. We assumed high quality graphene with a mobility of
 360 $\mu = 40000 cm^2/V * s$ (60). The gate voltages were converted to carrier sheet densities via
 361 $n_{L,R} = (0.73 * 10^{16} m^{-2} V^{-1})(V_{L,R} - V_{CNP})$. $V_{CNP} = 0.15V$ is the gate voltage at the charge neutrality
 362 point (CNP), which was determined by examining the gate dependence of the device. The
 363 coefficient $0.73 * 10^{16} m^{-2} V^{-1}$ was calculated as the static capacitance of the 27 nm thick hBN
 364 bottom layer with dielectric constant 3.56 (37).

365

366 **Antenna Theory**

367 The antenna impedance $Z_A = R_A + i * X_A$ was calculated using standard equations from RF
 368 antenna theory (45). The antenna resistance R_A (neglecting ohmic losses) and reactance X_A are
 369 given by

$$R_A = \frac{1}{2} \frac{\eta}{2\pi \sin\left(\frac{kl}{2}\right)^2} (C + \ln(kl) - C_i(kl) + \frac{1}{2} \sin(kl) (S_i(2kl) - 2S_i(kl)) + \frac{1}{2} \cos(kl) (C$$

$$+ \ln\left(\frac{kl}{2}\right) + C_i(2kl) - 2C_i(kl)))$$

370 and

$$X_A = \frac{1}{2} \frac{\eta}{4\pi \sin\left(\frac{kl}{2}\right)^2} (2S_i(kl)\cos(kl)(2S_i(kl) - S_i(2kl)) - \sin(kl)(2C_i(kl) - C_i(2kl)) - C_i\left(\frac{kD^2}{2l}\right))$$

371 where $C = 0.5772$ is the Euler constant, k is the wave vector of the electromagnetic wave, l is
 372 the antenna length, D is the antenna diameter, η is the impedance of the surrounding medium (for
 373 free space $\eta = 377\Omega$) and S_i and C_i are the sine and cosine integrals given by $S_i(z) =$
 374 $\int_z^\infty \frac{\sin(t)}{t} dt$ and $C_i(z) = \int_z^\infty \frac{\cos(t)}{t} dt$.

375

376 ASSOCIATED CONTENT

377 **Supporting Information.** The following files are available free of charge in the
 378 supplement (PDF).

379 - A detailed description of the fabrication process of the THz antenna tips used in this
 380 work.

381 - Scanning electron microscopy (SEM) images to measure the length of the probes.

382 - A description of the measurement of the linearity of the detector device.

383 - A Description of the Fourier filtering of the DC photocurrent signals.

384 - Numerical Calculation of the field confinement below the tip apex.

385

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389 Notes

390 The authors declare the following competing financial interest (s): R. Hillenbrand is co-founder
391 of Neaspec GmbH, a company producing scattering-type scanning near-field optical microscopy
392 systems such as the one used in this study. All other authors declare no competing financial
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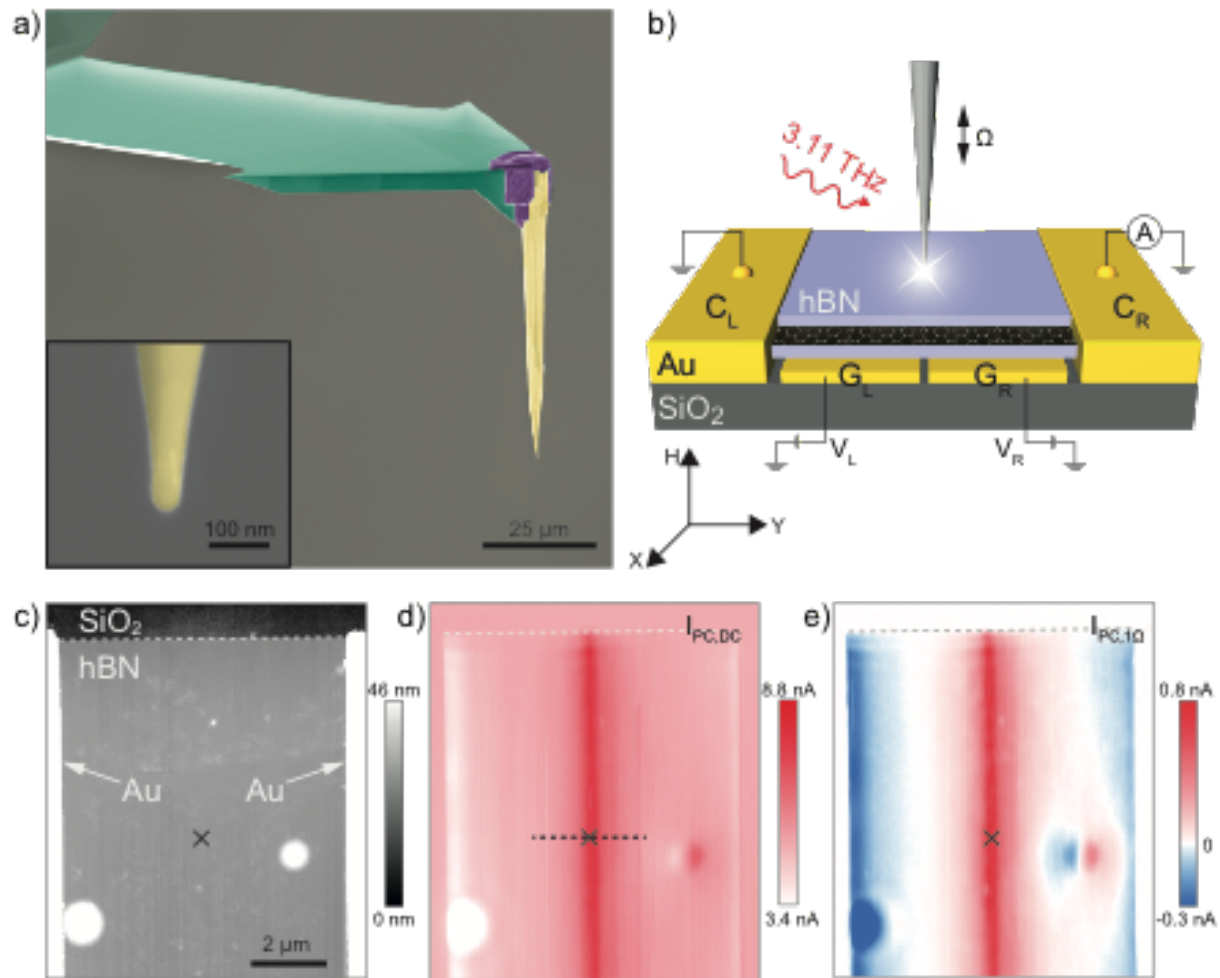
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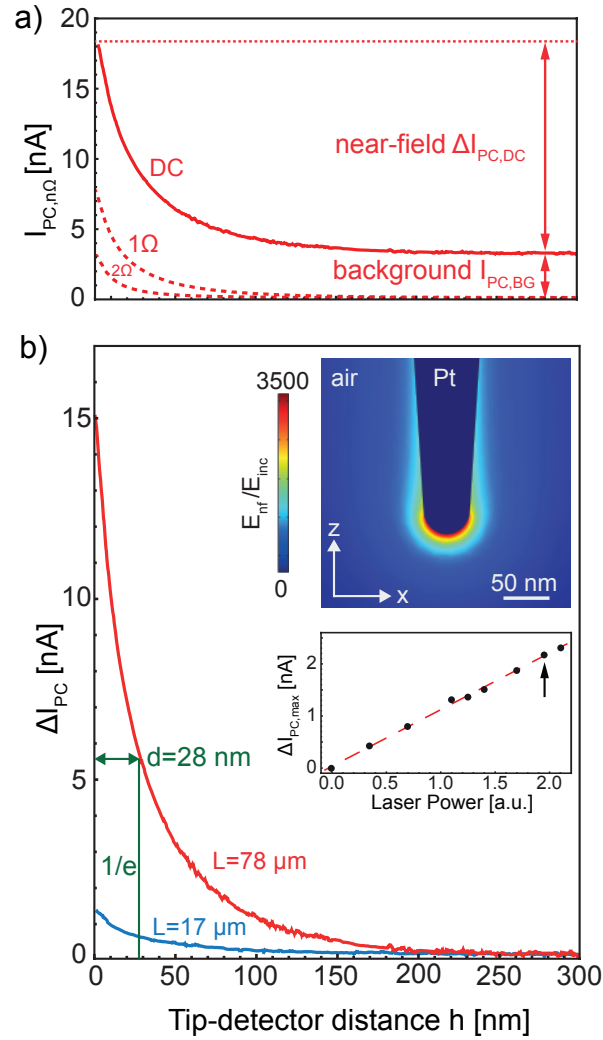
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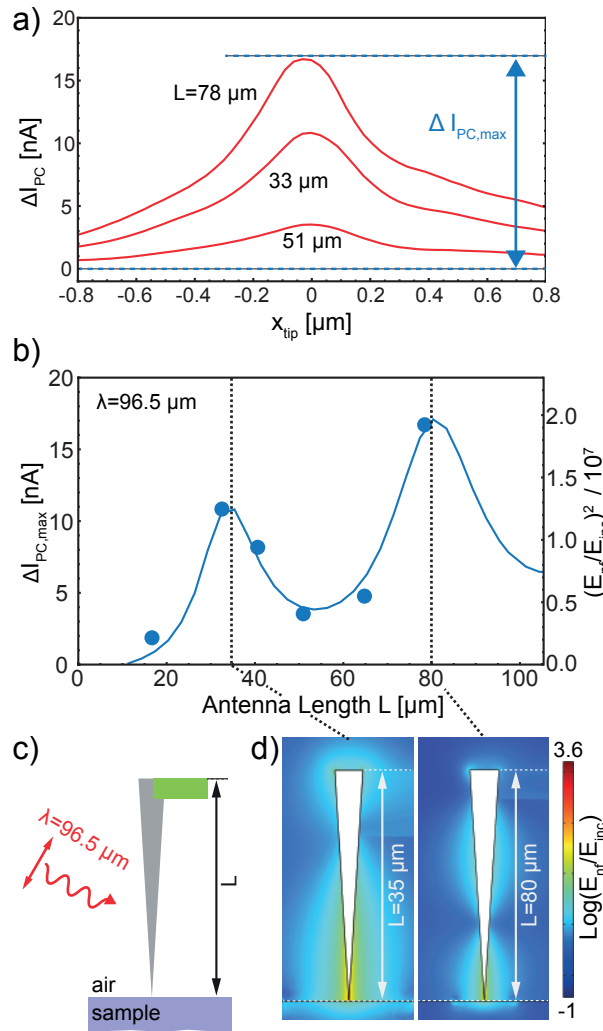
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 407 **Figure 1:** THz antenna tip and THz near-field detector: a) False color SEM
 408 fabricated THz antenna tip showing Si cantilever (green), focused ion beam deposited Pt
 409 (purple), and the Pt/Ir antenna tip (yellow). b) Schematics of the THz near-field detector. The
 410 laser illuminated antenna probe concentrates the light in the near-field region of the tip apex. The
 411 near-field induced photocurrent in the hBN-graphene-hBN heterostructure is detected through
 412 the two lateral contacts C_L and C_R . Applying voltages V_L and V_R to the two backgates G_L and G_R
 413 allow to separately control the carrier concentration in the graphene to the left and to the right of
 414 the gap between them. c) AFM topography image of the THz near-field detector. d) + e) Images
 415 of direct (photo-)current (DC) $I_{PC,DC}$ and photocurrent recorded at frequency 1Ω $I_{PC,1\Omega}$. The

416 white/gray dashed horizontal lines marks the edge of the graphene device. The black cross
417 identifies the position of the measured approach curves shown in Fig. 2. The horizontal dashed
418 black line marks the line profiles in Fig. 3.

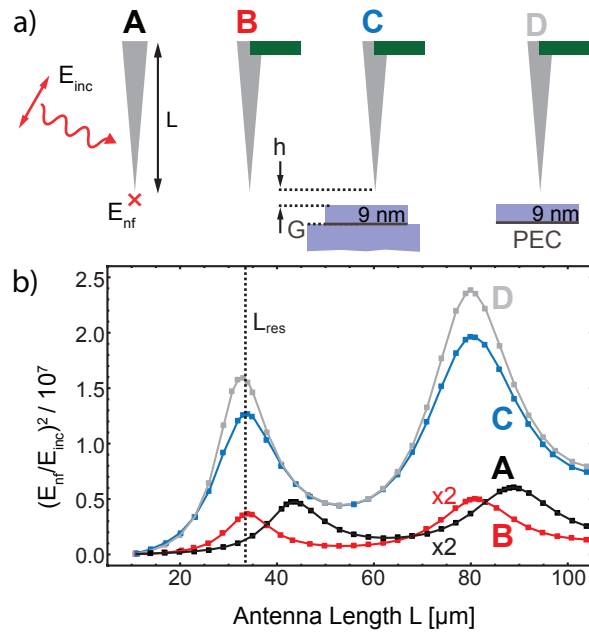


419

420 **Figure 2:** Photocurrent as a function of tip-detector distance. a) DC photocurrent $I_{PC,DC}$ and
 421 demodulated photocurrent $I_{PC,1\Omega}$ and $I_{PC,2\Omega}$. b) DC photocurrent after subtraction of background
 422 $\Delta I_{PC} = I_{PC,DC} - I_{PC,BG}$ for tips of lengths $L = 78 \mu\text{m}$ (red) and $17 \mu\text{m}$ (blue). The upper inset shows
 423 the numerically calculated electric field distribution around the apex of a $78 \mu\text{m}$ long antenna tip.
 424 The lower inset shows the measured linear dependence of the photocurrent ΔI_{PC} on the THz laser
 425 illumination power (black dots), and a linear least-squares fit to the data (red dashed line). The
 426 arrow marks the power applied in the experiment.



427
 428 **Figure 3:** Evaluation of signal strength for different THz antenna tips. a) Photocurrent ΔI_{PC} line
 429 profiles for antenna tips with length $33 \mu\text{m}$, $51 \mu\text{m}$, and $78 \mu\text{m}$. b) Maximum photocurrent
 430 $\Delta I_{PC,max}$ as a function of antenna length (blue dots) compared to numerical simulation (blue solid
 431 line). The vertical axes of the numerical simulation was manually adjusted such that best
 432 agreement to the experimental data points was obtained. c) Sketch of numerically simulated
 433 geometry (see more detail in Fig. 4a C) showing the tip (gray), the silicon cantilever (green), and
 434 the detector device (purple). d) False color image of the logarithm of the electric field
 435 enhancement of tips of length $L = 35 \mu\text{m}$ and $80 \mu\text{m}$, showing the first and second fundamental
 436 antenna resonance.



437

438 **Figure 4:** Evaluation of peak position of fundamental antenna resonances. a) Antenna

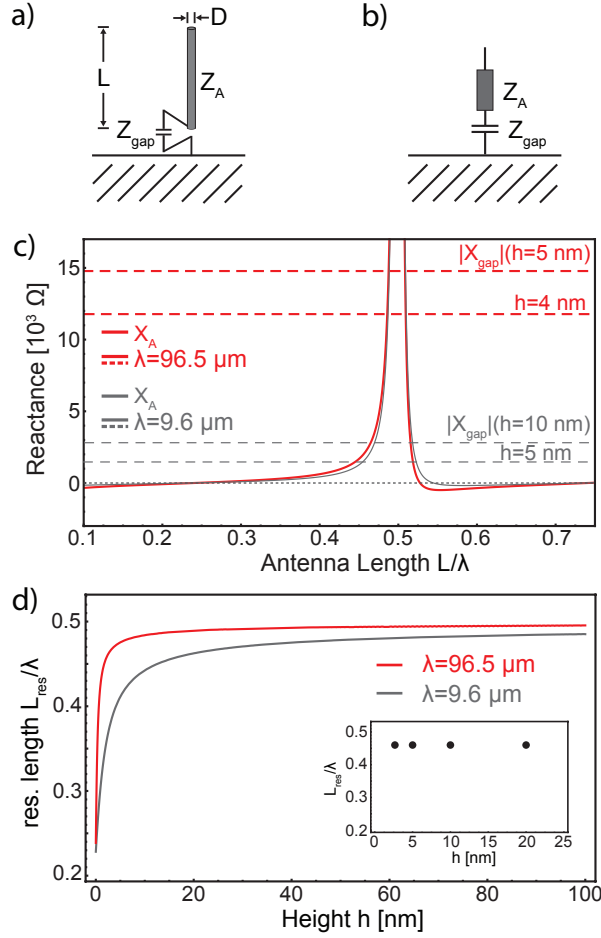
439 geometries considered in the simulation. A: conical antenna tip. B: antenna tip with Si cantilever.

440 C: as in B but with detector device below (9 nm hBN-graphene-bulk hBN) tip apex. D: as in C,

441 replacing graphene with a PEC. b) Simulated antenna spectra for geometries A – D depicted in

442 Fig. 4a.

443



444

445 **Figure 5:** a, b) RF circuit model of a linear wire antenna above ground with input impedance Z_{in} ,

446 antenna impedance Z_A , and gap impedance Z_{gap} . c) Antenna reactance X_A (solid lines) and gap

447 reactance X_{gap} (dashed lines) as a function of antenna length L for wavelength $\lambda = 96.5 \mu\text{m}$ (red)

448 and $\lambda = 9.6 \mu\text{m}$ (black). d) Antenna resonance length L_{res} normalized to the excitation

449 wavelength λ as a function of gap width h . The inset shows a numerical calculation of the

450 resonance length L_{res} for a THz antenna tip above a PEC.

451